

4 - Mode structure - laser resonators

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4.(a) - Generalities

- ④ So far: We have concentrated on the materials used in a laser \Rightarrow the laser frequency may be chosen by fixing a particular transition
 - We have also seen that line broadening occurs for several reasons (Doppler broadening, finite lifetimes, pressure broadening, etc.)
- ④ Solution: One may select frequencies further using resonators

④ Ideal situation: cavity whose walls have an ~~infinitely~~ infinitely high conductivity
 \Rightarrow standing waves at discrete frequencies

④ Lasers:

- Open sides \Rightarrow diffraction losses \Rightarrow Are stationary modes possible?
- Mirrors \Rightarrow transmission losses
- First (numerical) proof: A. G. Fox and T. Li, Bell Sys. Tech. J. 40, 453 (1961); Proc. IEEE 51, 80 (1963)

They found modes whose intensity decreased due to losses in the cavity, but whose shape remained the same.

* Important issues (modes in a laser cavity)

- Modes have a finite lifetime \Rightarrow frequency width
 - Good cavity: mode widths \ll atomic linewidths
 - Bad cavity: mode widths \gg atomic linewidths
- Apart from the longitudinal modes in a cavity, there exist also transverse modes. They come from the fact that the waves propagating inside the cavity exhibit a transverse intensity variation (further distortions due to the specific geometry of the cavity, such as refractive indices of lenses, etc. are also present).
- Let us consider the field

$$E(x, y, z) = \text{Re} \left[E(x, y, z) e^{i(\omega t - kz) + i\phi(x, y, z)} \right]$$

We are looking for transverse patterns $E_{n,m}(x, y, z_0)$ at $z = z_0$ such that, if the field starts with that pattern, after a round trip in the cavity it will exhibit the same pattern at $z = z_0$

- The field components will be primarily polarized transverse to the propagation direction
 $\Rightarrow TE M_{nm}$ (transverse electric modes)

- This type of propagation occurs, for instance, in confocal resonators formed by spherical mirrors
- The transverse modes of a light beam propagating along the \vec{z} axis of the cavity are given by

$$E_{mm} = E_0 H_m\left(\frac{x\sqrt{2}}{w}\right) H_m\left(\frac{y\sqrt{2}}{w}\right) e^{-\frac{(x^2+y^2)}{w^2}}$$

↓ ↓
Hermite Gaussian beam
polynomials

with w = spot size

* Starting point: wave equation (gives the propagation of the field)

For our purposes, we can consider the field as a scalar

$$\Delta U = \left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} \right) U = \frac{1}{c^2} \frac{\partial^2 U}{\partial t^2} \quad (*)$$

Monochromatic wave : $U(\vec{r}, t) = U(\vec{r}) e^{i\omega t}$

$$(*) \Rightarrow \Delta U + k^2 U = 0, \quad k = \frac{\omega}{c}$$

* Assumptions

- The wave is propagating in the \vec{z} direction

$$\Rightarrow U(x, y, z) = f(x, y, z) e^{-ikz}$$

↓ ↓
related to related to the propagation
the fact that f changes with z

- The transverse dependence determines the beam profile
- $\lim_{\substack{x \rightarrow \infty \\ y \rightarrow \infty}} f(x, y, z) = 0$
- Paraxial approximation

$$\left| \frac{\partial^2 f}{\partial z^2} \right| \ll \left| \frac{\partial^2 f}{\partial x^2} \right| + \left| \frac{\partial^2 f}{\partial y^2} \right|, k^2 f$$

$$\frac{\partial^2 U}{\partial z^2} = \frac{2}{\partial z} \left(\frac{\partial f}{\partial z} e^{-ikz} - ikf e^{-ikz} \right)$$

$$= \frac{\partial^2 f}{\partial z^2} e^{ikz} - 2ik \frac{\partial f}{\partial z} e^{-ikz} - k^2 f e^{-ikz}$$

✓

neglected

$$\Rightarrow (*) = \frac{\partial^2 f}{\partial x^2} + \frac{\partial^2 f}{\partial y^2} - 2ik \frac{\partial f}{\partial z} = 0$$

④ Ansatz : $f(x, y, z) = X(x) Y(y) G(z) \exp\left(-\frac{x^2 + y^2}{F(z)}\right)$

$F(z)$, $G(z)$ slowly varying

(yields $\lim_{\substack{x \rightarrow \infty \\ y \rightarrow \infty}} f(x, y, z) = 0$)

For a justification of why taking a Gaussian dependence based on the Huygen's principle see Haken, laser light dynamics, p. 49.

Inserting in Eq. (*) :

$$\begin{aligned} \frac{\partial^2 f}{\partial x^2} &= Y(y) G(z) \frac{\partial}{\partial x} \left(\frac{dX}{dx} e^{-\frac{x^2+y^2}{F}} - \frac{2x}{F} X e^{-\frac{x^2+y^2}{F}} \right) \\ &= \left(\frac{d^2 X}{dx^2} - \frac{4x dX}{F} - \frac{2}{F} X + \frac{4x^2}{F^2} X \right) Y(y) G(z) e^{-\frac{x^2+y^2}{F}} \end{aligned}$$

Similarly,

$$\frac{\partial^2 f}{\partial y^2} = X(x) G(z) \left(\frac{d^2 Y}{dy^2} - \frac{4y}{F} \frac{dY}{dy} - \frac{2}{F} Y + \frac{4y^2}{F^2} Y \right) e^{-\frac{x^2+y^2}{F}}$$

$$\frac{\partial f}{\partial z} = X Y \left(\frac{dG}{dz} e^{-\frac{x^2+y^2}{F}} + G(z) \frac{x^2+y^2}{F^2(z)} \frac{dF}{dz} e^{-\frac{x^2+y^2}{F}} \right)$$

Inserting in (*) and dividing by $X Y G e^{-\frac{x^2+y^2}{F}}$

yields

$$\frac{1}{X} \frac{d^2 X}{dx^2} - \frac{4x}{F} \frac{dX}{dx} - \frac{2}{F} + \frac{4x^2}{F^2} + \frac{1}{Y} \frac{d^2 Y}{dy^2} - \frac{4y}{F} \frac{1}{Y} \frac{dY}{dy} - \frac{2}{F} + \frac{4y^2}{F^2}$$

$$- 2ik \left(\frac{1}{G} \frac{dG}{dz} + \frac{(x^2+y^2)}{F^2} \frac{dF}{dz} \right) = 0$$

Regrouping,

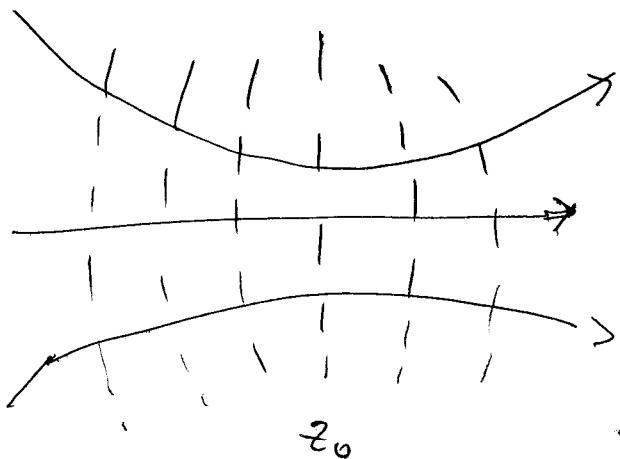
$$\left(\frac{1}{X} \frac{d^2 X}{dx^2} - \frac{4x}{F} \frac{dX}{dx} \right) + \left(\frac{1}{Y} \frac{d^2 Y}{dy^2} - \frac{4y}{F} \frac{dY}{dy} \right) - \frac{4}{F} - \frac{2ik}{G} \frac{dG}{dz} + \left(+ 2 \frac{(x^2+y^2)}{F^2} \left(2 - ik \frac{dF}{dz} \right) \right) = 0$$

One underlying assumption is that F does not depend on x or y (otherwise it would influence the shape of the beam).

Hence, the last term must vanish

$$\Rightarrow \frac{dF}{dz} = \frac{2}{ik} \quad F(z) = \frac{2}{ik} (z + C)$$

Assumption: we will have a plane wavefront for $z = z_0$



$$\frac{2}{ik} (z_0 + c) = \omega_0^2 \Rightarrow c = \frac{ik\omega_0^2 - z_0}{2}$$

$$\Rightarrow F(z) = \omega_0^2 + \frac{2}{ik} (z - z_0)$$

ω_0 = minimal beam radius

This implies that the phase at z_0 cannot depend on x, y
 $\Rightarrow F(z_0)$ Real = ω_0^2
 and also that

$$x^2 + y^2 = \omega_0^2 \quad (\text{otherwise we will find a gaussian dependence on } x, y)$$

Let us now consider the remaining terms

$$\underbrace{\frac{1}{X} \frac{d^2 X}{dx^2} - \frac{4X}{F(z)} \frac{dX}{dx}}_{I} + \underbrace{\frac{1}{Y} \frac{d^2 Y}{dy^2} - \frac{4Y}{F(z)} \frac{dY}{dy}}_{II} - \left[\frac{4}{F(z)} + 2ik \frac{dG/dz}{G} \right] = 0$$

The above-stated equation only holds if one can find three constants, or at most functions of F_j whose sum vanishes.

If we choose $I = -\frac{4m}{F}$; $II = -\frac{4n}{F}$ then $III = \frac{4(m+n)}{F}$

$$\Rightarrow \frac{4}{F} + \frac{2ik}{G} \frac{dG}{dz} = -\frac{4(m+n)}{F}$$

$$\frac{2ik}{G} \frac{dG}{dz} = -\frac{4(m+n+1)}{F} = -\frac{4ik(m+n+1)}{F(z+c)}$$

$$\Rightarrow \frac{dG}{G} = -(m+n+1) \frac{dz}{z+c}$$

$$\Rightarrow \ln G = -(n+m+1) \ln(z+c) + c_2$$

$$G = \frac{A}{(z+c)^{n+m+1}}$$

Other variables:

$$\frac{1}{X} \frac{d^2X}{dx^2} - \frac{4x}{F(x)} \frac{dX}{dx} = -\frac{4m}{F} \Rightarrow X(x) = H_m \left(\sqrt{\frac{2}{F}} x \right)$$

$$\frac{1}{Y} \frac{d^2Y}{dy^2} - \frac{4y}{F(y)} \frac{dY}{dy} = -\frac{4m}{F} \Rightarrow Y(y) = H_m \left(\sqrt{\frac{2}{F}} y \right)$$

$$U_{mm}(x, y, z) = H_m \left(\sqrt{\frac{2}{F}} x \right) H_m \left(\sqrt{\frac{2}{F}} y \right) \frac{A}{(z+c)^{n+m+1}} e^{-\frac{(x^2+y^2)}{F} + ikz}$$

(*) Physical interpretation

Let us consider the exponential factor

$$\exp \left\{ -\operatorname{Re} \left(\frac{1}{F} \right) (x^2+y^2) - i [kz + \operatorname{Im} \left(\frac{1}{F} \right) (x^2+y^2)] \right\}$$

If we define $z_R = \frac{\omega_0^2 k}{2} = \omega_0^2 \frac{\pi}{\lambda}$ then

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$$F(z) = \frac{2}{k} \left[z_R - i(z-z_0) \right]$$

↑
Rayleigh length

$$\frac{1}{F(z)} = \frac{k}{2} \frac{z_R + i(z-z_0)}{z_R^2 + (z-z_0)^2}$$

• Beam Radius $\omega(z)$ $\Rightarrow \omega^2(z) = \frac{1}{\operatorname{Re}\left(\frac{1}{F}\right)}$ so that

the real part of the exponential reads $\frac{x^2+y^2}{[\omega(z)]^2}$

$$\begin{aligned} \omega^2(z) &= \frac{1}{\operatorname{Re}\left(\frac{1}{F}\right)} = \frac{2}{k} \left(z_R + \frac{(z-z_0)^2}{z_R} \right) = \frac{2}{k \omega_0^2 \pi} \cdot \frac{\pi^2 \omega_0^2}{\lambda^2} \left(1 + \frac{(z-z_0)^2}{z_R^2} \right) \\ &= \cancel{\frac{2\pi}{1}} \cdot \frac{1}{\omega_0^2} \left(1 + \frac{(z-z_0)^2}{z_R^2} \right) \end{aligned}$$

$z-z_0 \ll z_R \Rightarrow$ one can neglect the broadening in the beam. The smaller ω_0 is, the shorter z_R (small aperture, large diffraction angle).

• Curvature R of the wavefront

$$\exp \left[-ik \left(z + \operatorname{Im}\left(\frac{1}{F}\right) \right) \frac{x^2+y^2}{k} \right] = \exp \left[-ik \left(z + \frac{x^2+y^2}{2R} \right) \right]$$

$$R = \frac{k}{2} \frac{1}{\operatorname{Im}\left[\frac{1}{F}\right]} = (z-z_0) + \frac{z_R^2}{(z-z_0)} \quad \text{(Curvature of the wavefront at the position } z)$$

$z = z_0 \Rightarrow$ plane wave

* Please note

- The arguments of the Hermite polynomials are complex \Rightarrow together with $\frac{1}{(z+c)^{n+m+1}}$ they give the conditions for the eigenmodes in the resonator
- Transverse modes:
- Ground mode: $n=m=0 \Rightarrow$ gaussian intensity profile
- Higher-order modes: the intensity profile is broader \Rightarrow larger energy loss
- Normally one selects the ground transverse mode
 \Rightarrow higher modes lead to a messy output
- One may form a resonator by inserting at the points z_1, z_2 two reflectors with radii r of curvature that match those of the propagating beam phase fronts at these points
- Alternatively, given two mirrors, one can adjust the positions z_0 , and w_0 so that the mirrors coincide with the wavefronts

* Resonance condition - longitudinal modes

Let us consider the phases of a wave at $z = z_1$
and $z = z_2$

$$e^{-i\phi_1} = \frac{e^{-ikz_1}}{(z_1 - z_0 + iz_R)^{n+m+1}}$$

$$e^{-i\phi_2} = \frac{e^{-ikz_2}}{(z_2 - z_0 + iz_R)^{n+m+1}} = \frac{e^{-ikz_1}}{(z_1 - z_0 + iz_R)^{n+m+1}} \frac{e^{ik(z_1 - z_2)}}{\frac{(z_1 - z_0 + iz_R)^{n+m+1}}{(z_2 - z_0 + iz_R)^{n+m+1}}}$$

Let us also call

$$\alpha = \frac{z_1 - z_0 + iz_R}{z_2 - z_0 + iz_R}, \phi_0 = \text{Arg } \alpha$$

$$\Rightarrow e^{-i\phi_2} = e^{-i\phi_1 + i\Delta\phi}$$

with $i\Delta\phi = k(z_1 - z_2) + (n+m+1)\phi_0$

Resonance condition: the wave has to have the same phase after a round-trip in the cavity

$$\Rightarrow \Delta\phi = m\pi$$

Depends on the cavity. Details: Yariv, Chapter 7

$$k(z_1 - z_2) + (n+m+1)\phi_0 = m\pi$$

If, for simplicity, we had a plane wave, the above-stated condition would reduce to

$$k(z_1 - z_2) = n\pi \quad z_1 - z_2 = l \text{ (cavity length)}$$

Frequency difference between two consecutive modes:

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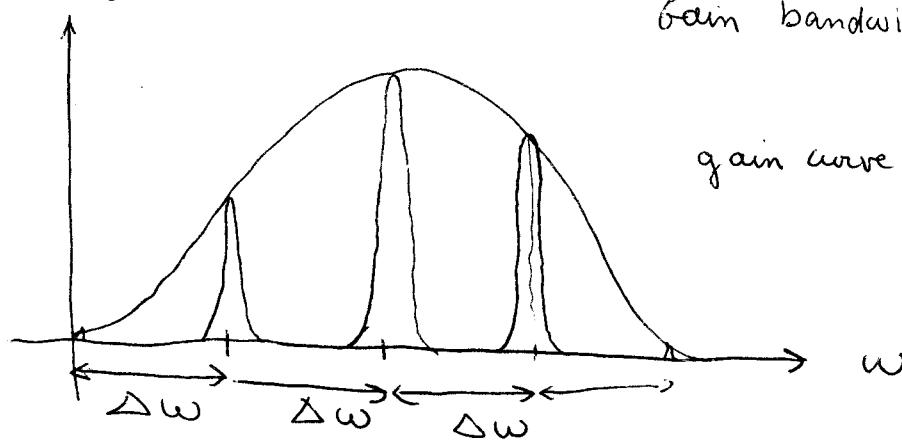
$$\omega_n l = n\pi c \Rightarrow \Delta\omega = \frac{\pi c}{l}$$

$$\omega_{n+1} l = (n+1)\pi c$$

Please note: these modes will also exhibit a linewidth
(the cavity is an open system, there are losses, etc)

Example

Generic case:



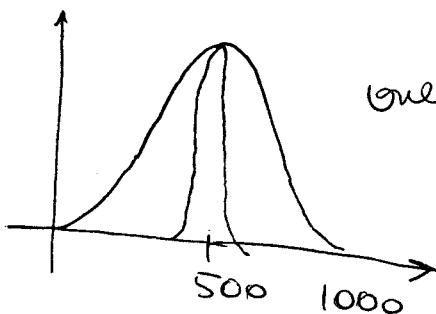
Gain bandwidth = range of frequencies a laser may operate over

gain curve $g(\omega)$

3 modes oscillate

He-Ne laser: gain curve dopples broadened 1000 MHz

$$\Delta\omega = \frac{c\pi}{l} \quad \Rightarrow \Delta\omega = 500 \text{ MHz}$$



only one mode oscillates